

Co-Firing Coal/Biomass And The Estimation Of Burnout And NO_x Formation

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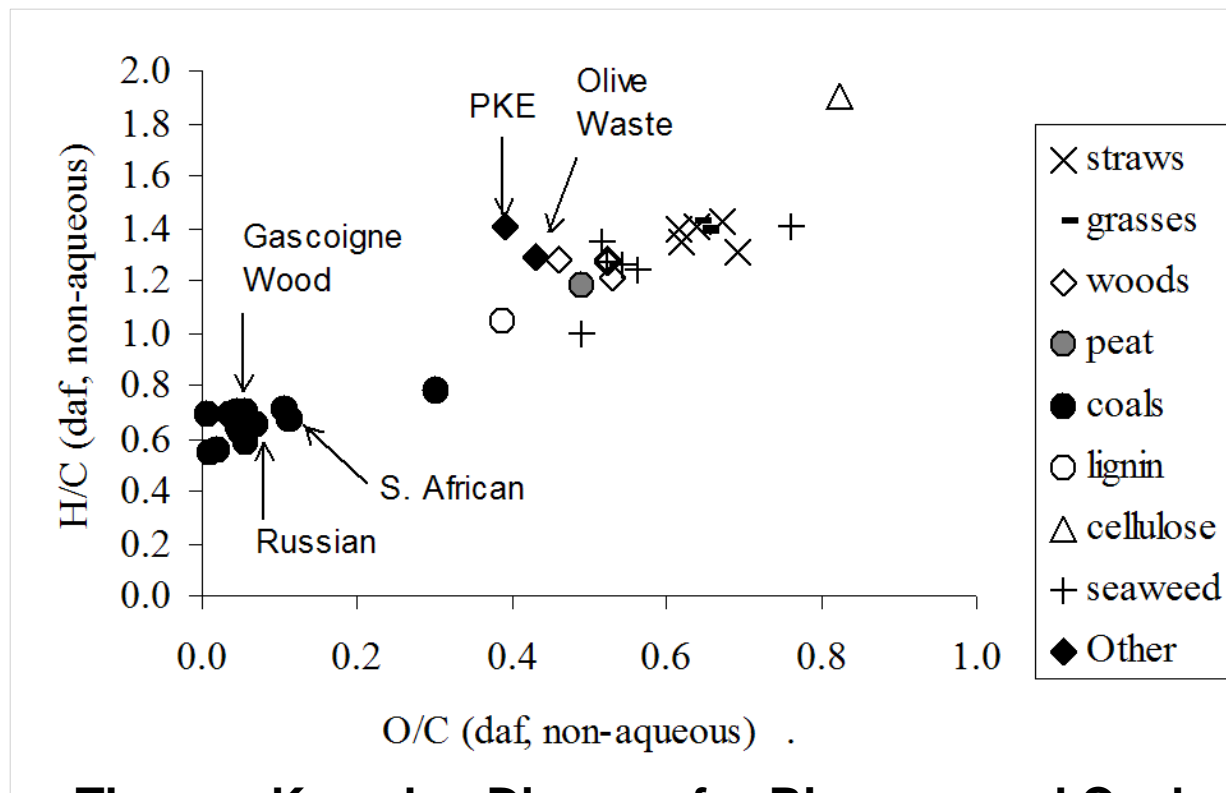
Co-firing is widely used in UK power stations.

**The biomass does not mill as well as coal
and can lead to larger particles.**

**There are uncertainties about the
mechanism of the formation of NO when
biomass is present.**

1. Gascoigne Wood (GW) coal- used as a test coal for the CFD model
2. Russian coal
3. Russian/PKE
4. S. African coal
5. S. African coal/milled wood(20% thermal)
6. S. African/Miscanthus Giganteus (20% thermal)
7. S. African/ Olive waste (15% thermal)
8. S. African/Torrefied wood (20% thermal)

Experimental data: exit NO, T and C-in-ash, and data on radiation and flame properties for GW coal



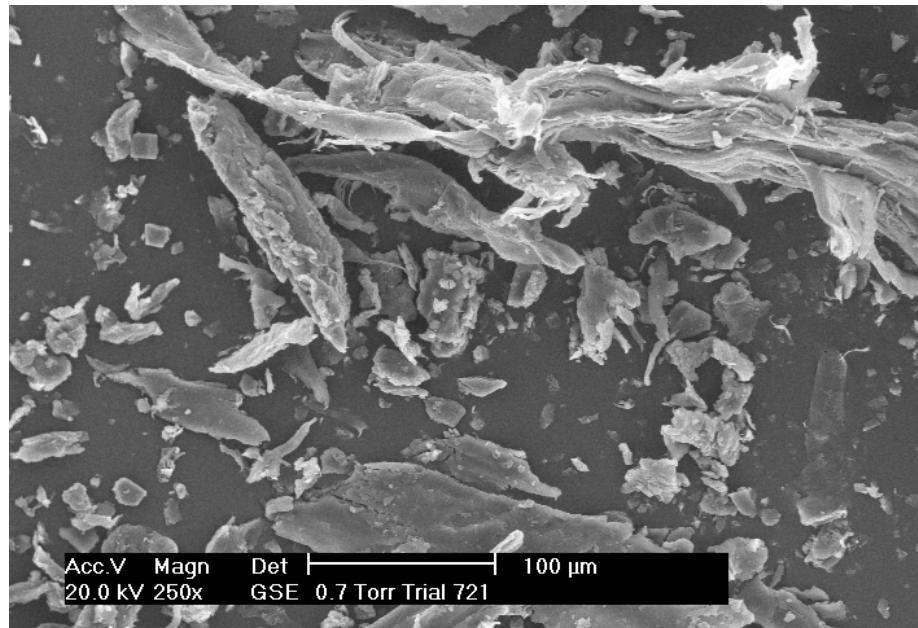
The van Krevelen Diagram for Biomass and Coal.

*Coals and most biomass have conventional properties-
PKE and Olive waste are different*

Milled Wood.



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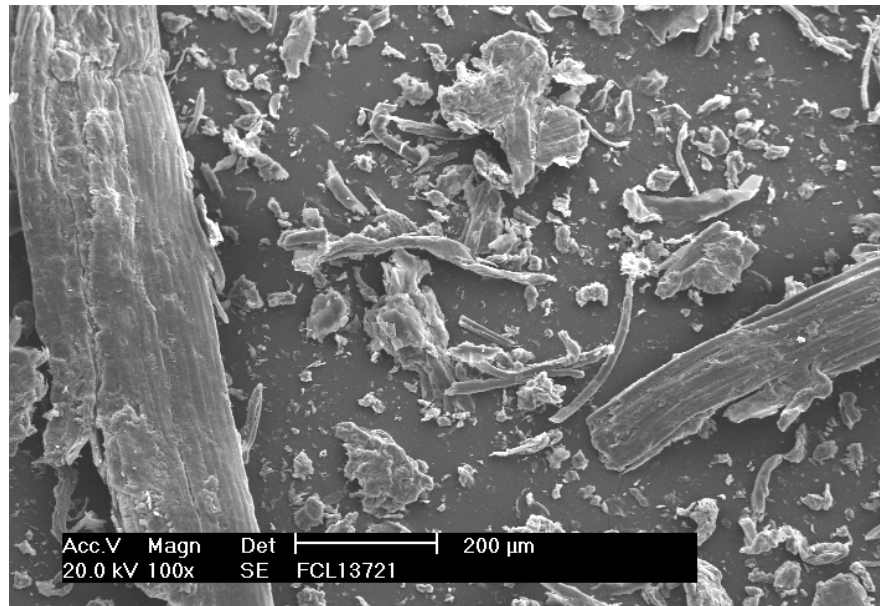


Milled Wood

Miscanthus.



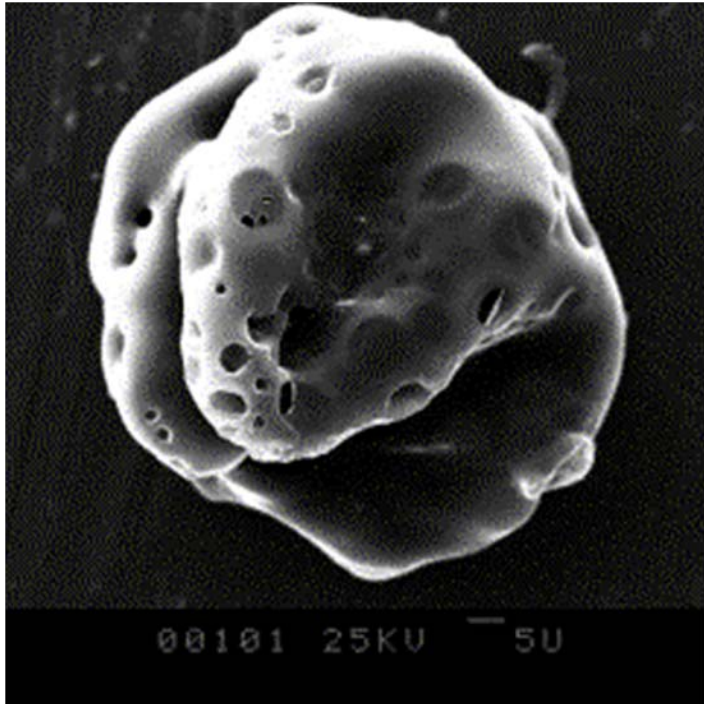
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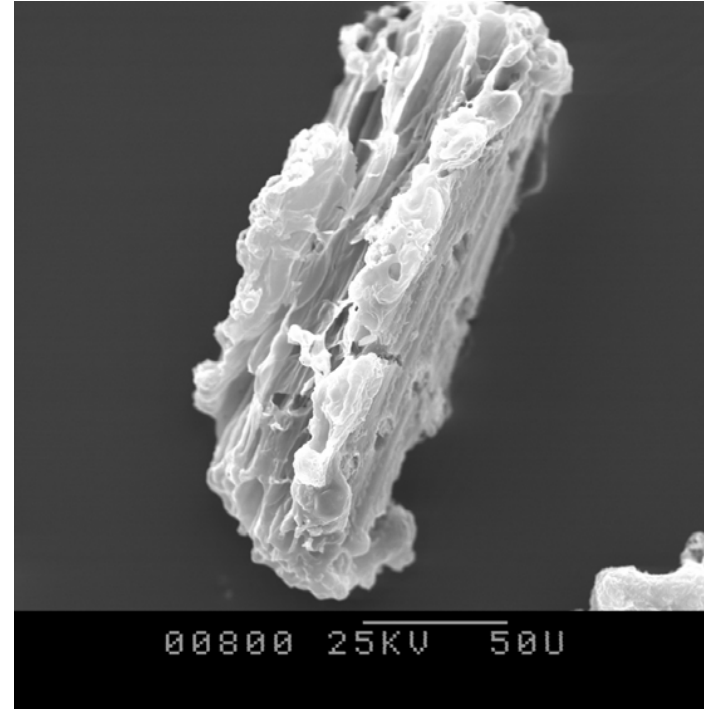
Miscanthus

Biomass combustion: particle shape is complex.

Coal



Wood

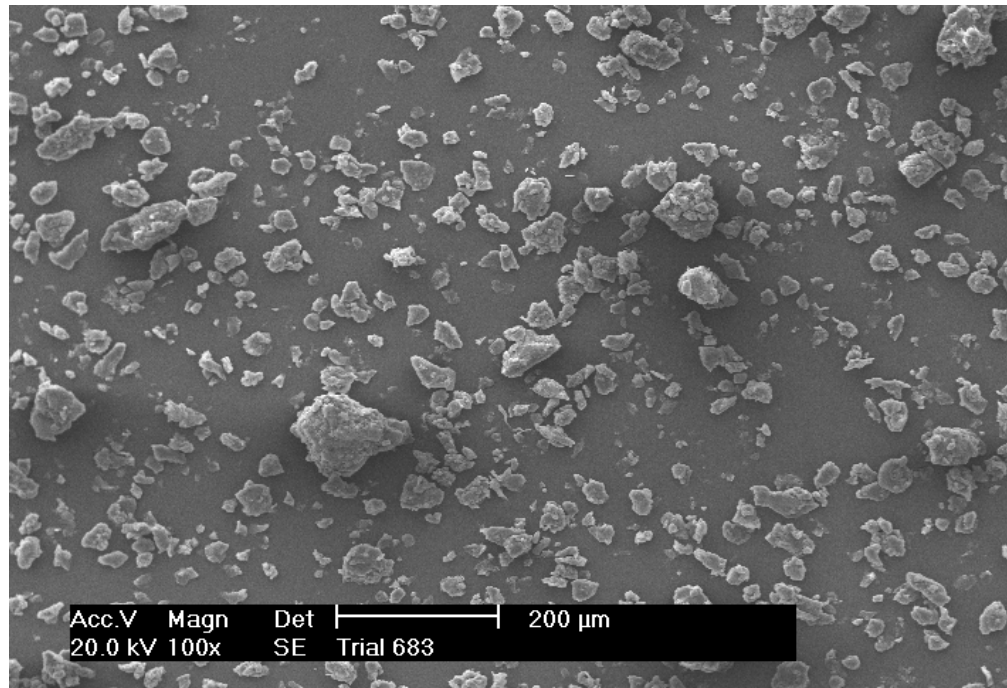


Complex drag coefficients. Shape factor given by:
 $f = \{\text{surface area equivalent sphere}\} / \{\text{actual surface area}\}$

Palm Kernel Extractor.



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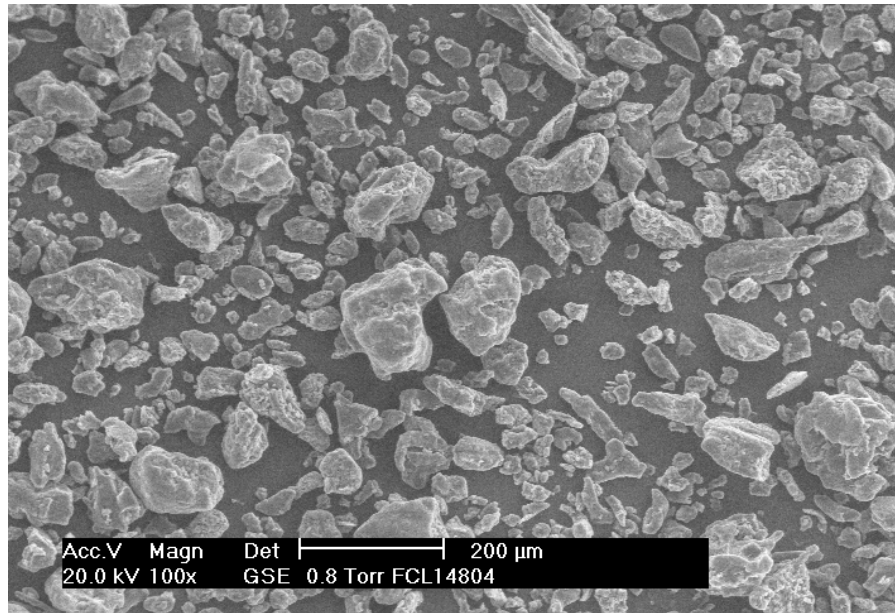


PKE

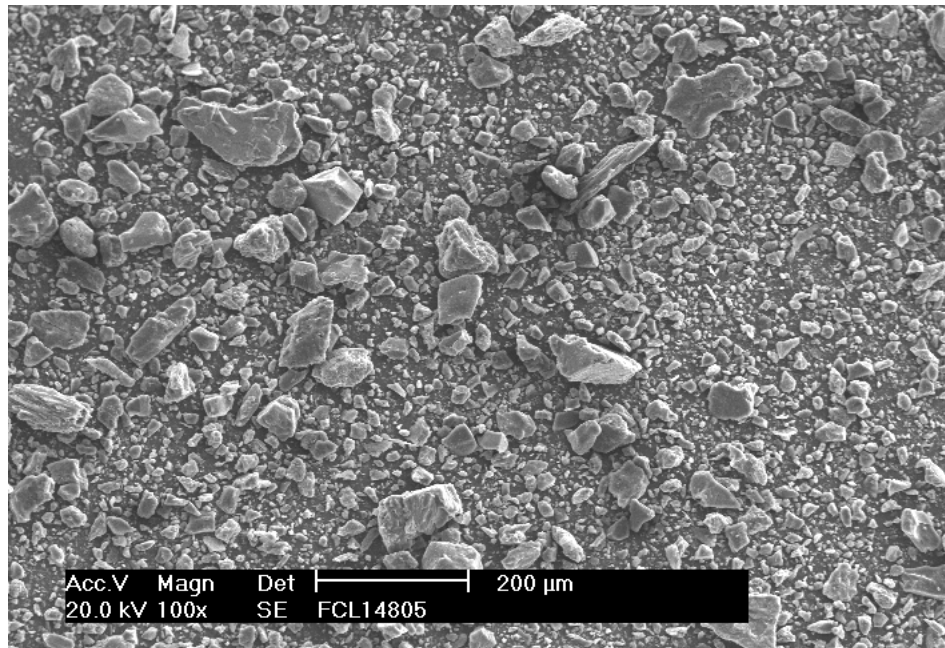
Olive Waste.



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Olive Waste



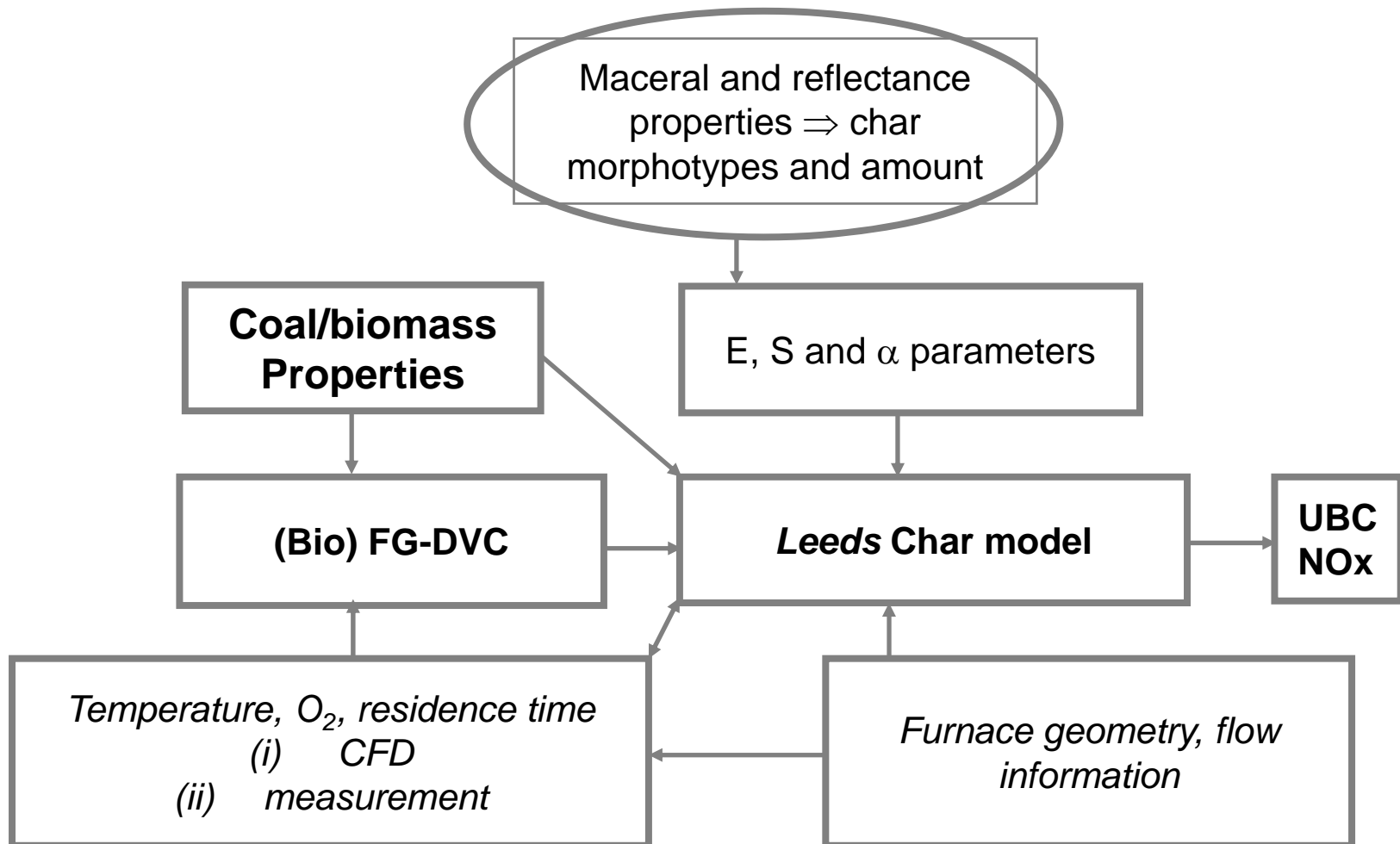
Blend of South African coal and 15% Olive waste



and soot formation and burnout.

A potassium release mechanism can be added if required.

Coal/biomass BURNOUT MODEL



Devolatilisation Rates of Coal.



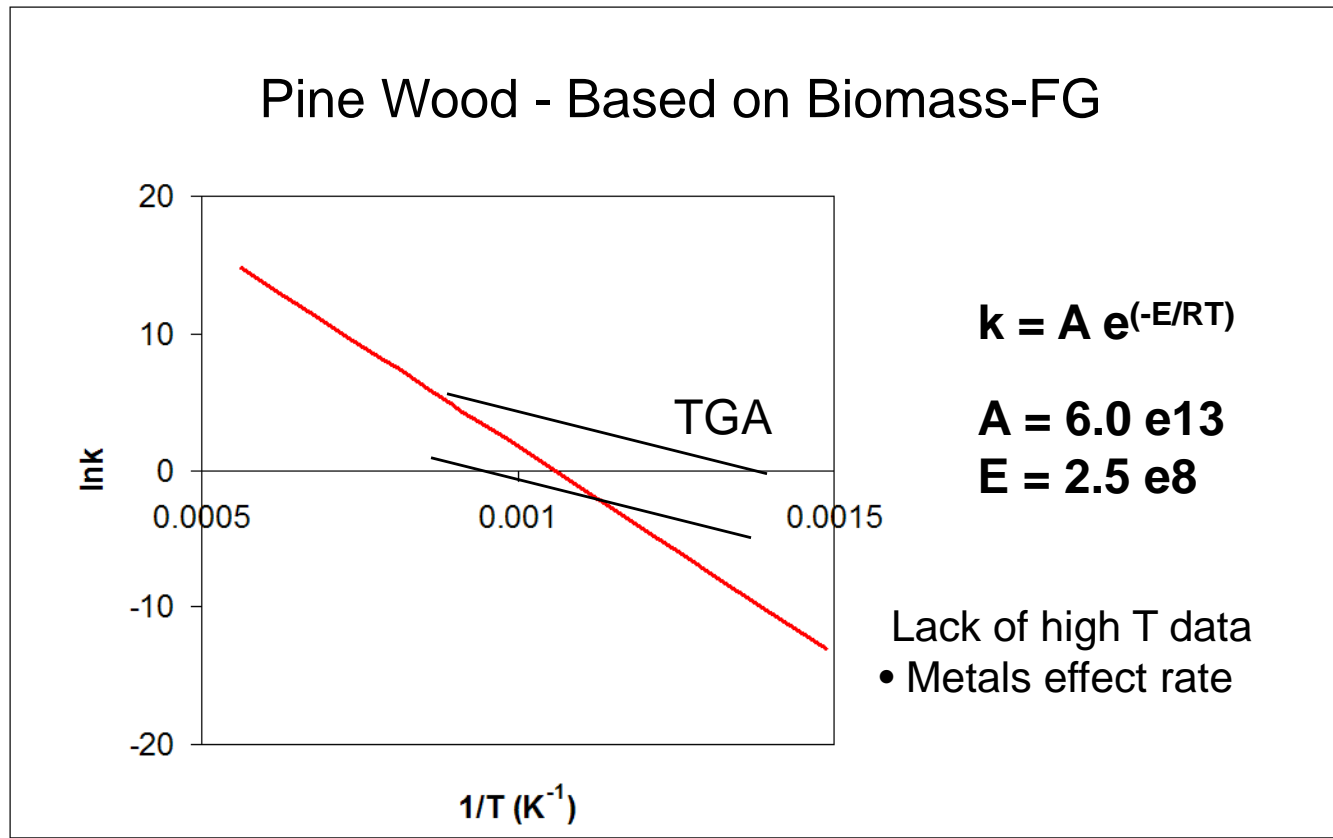
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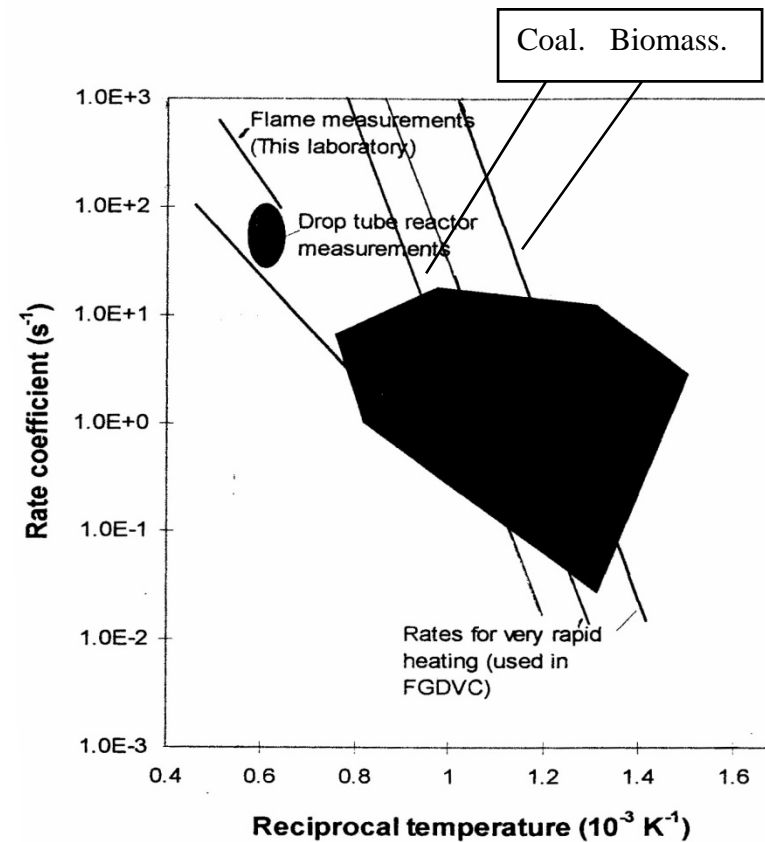
Coal (Origin)	Devolatilisation Rates – FG-DVC computed					
	Activation Energy, E_d (J/kmol)			Pre-Exponential factor, A_d (s^{-1})		
	Tar	Gas	Total	Tar	Gas	Total
Thoresby	3.3×10^8	2.4×10^8	2.4×10^8	3.8×10^{14}	4.6×10^{13}	5.2×10^{14}
Asfordby	2.0×10^8	2.1×10^8	2.3×10^8	3.7×10^{14}	4.2×10^{13}	4.8×10^{14}
Betts Lane	2.5×10^8	2.3×10^8	2.4×10^8	2.1×10^{14}	3.2×10^{12}	3.3×10^{14}
Pittsburgh#8	2.3×10^8	2.2×10^8	2.3×10^8	3.7×10^{14}	4.8×10^{12}	3.8×10^{14}
Ensham	2.4×10^8	2.7×10^8	2.4×10^8	4.1×10^{14}	3.2×10^{14}	4.3×10^{14}
Prodeco	2.3×10^8	2.4×10^8	2.4×10^8	3.0×10^{14}	4.6×10^{13}	5.2×10^{14}

We used an averaged value for all coals.

A similarly high value was used for biomass

Biomass Devolatilisation Kinetics.





Summary of Kinetic Analysis

The use of rapid rates implies that the controlling step is the heating-up process, T , C_p important.

Volatile Yields of the Coals Studied.



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Volatile Yields (%wt, daf)

Coal	VM (daf)	Calculated, FG-DVC	Values from RWE npower	Experimental values: CRE, 1350° C
Gascoigne Wood coal	35.11	55.1	55.5%	48.7
Russian coal	43.43	58.1	57.5 - 69.5*	58.3
South African	37.64	54.75	48.9 - 60.2*	49.92

•From Man et al., Fuel, 2005

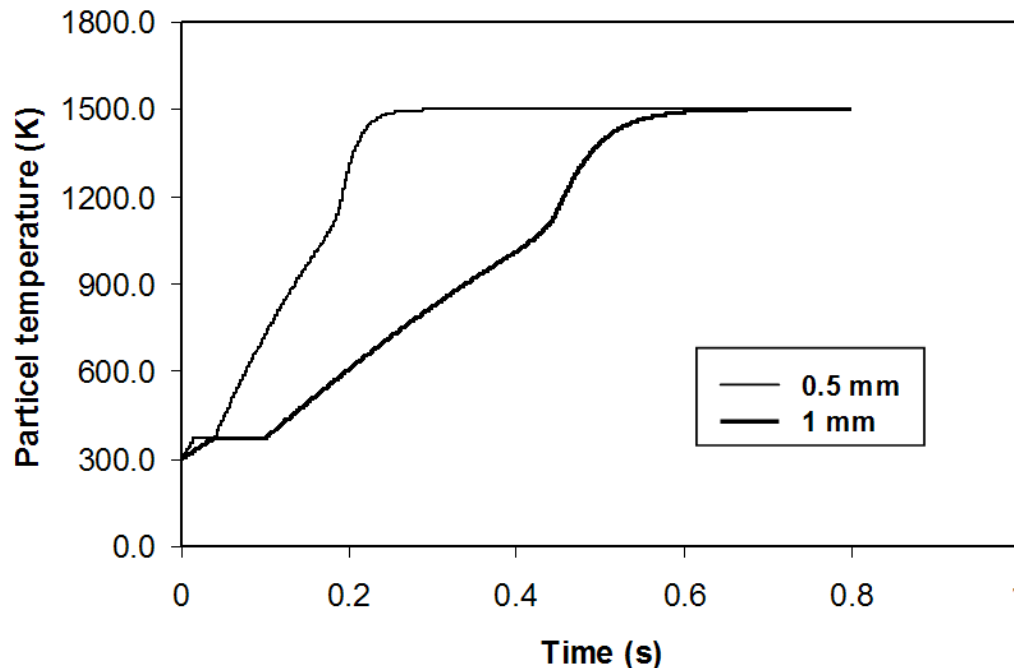
Volatile Yields (daf)

Biomass	VM (daf)	Calculated by Bio-FG	Value given by RWE npower
Milled wood	86.58.7	90.91	76.34
PKE	93.13	97.79	85.54
Olive	75.71	79.50	
Miscanthus	80.8	84.8	
Torrefied wood	75	80	

Heating-up Curves for Large Biomass Particles.



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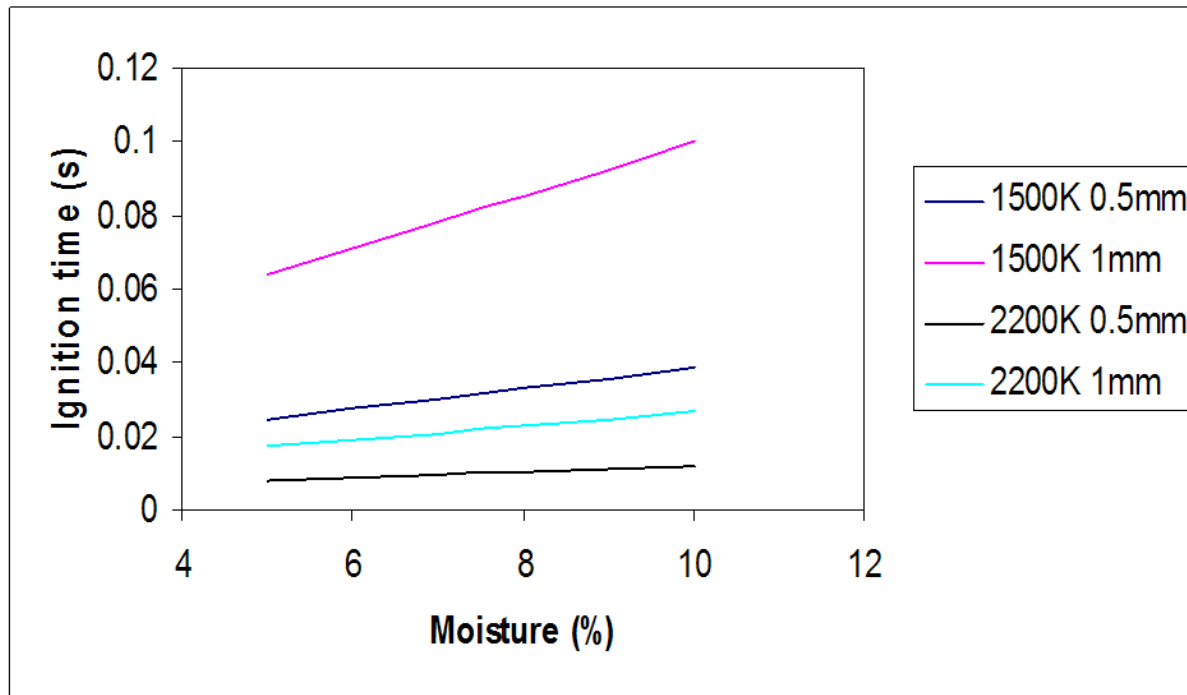
**Heating-up Curves for Biomass Particles,
(0.5 and 1 mm diam, 5% water content).**

C_p and the water content are important

Effect of Moisture Content on Biomass Ignition.



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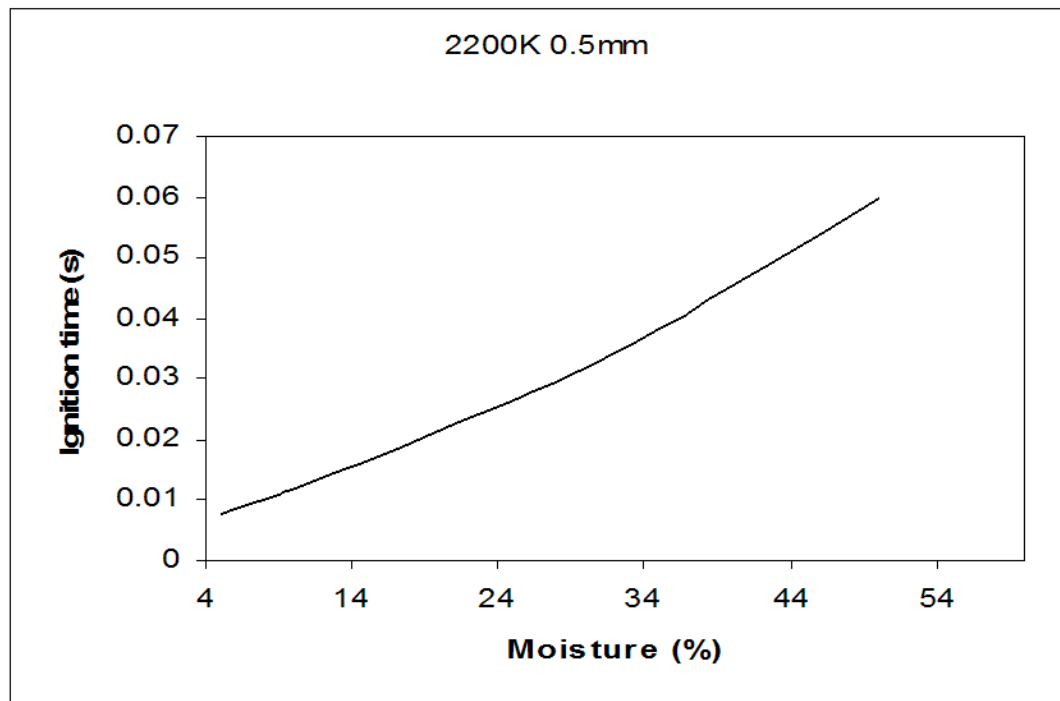


Time to Ignition (taken as the end of water evaporation) as a function of moisture content for different sized particles and temperature.

Effect of High Moisture Content.



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Ignition times for high moisture levels, 0.5 mm and 2200K.

The formation of soot was estimated by the equation below-

$$\mathcal{R}_{\text{soot,form}} = C_s p_{\text{fuel}} \phi^r e^{-E/RT}$$

The combustion of the soot particles was governed by the Magnussen equation.

RWE npower CTF



Modelling the RWE npower CTF.



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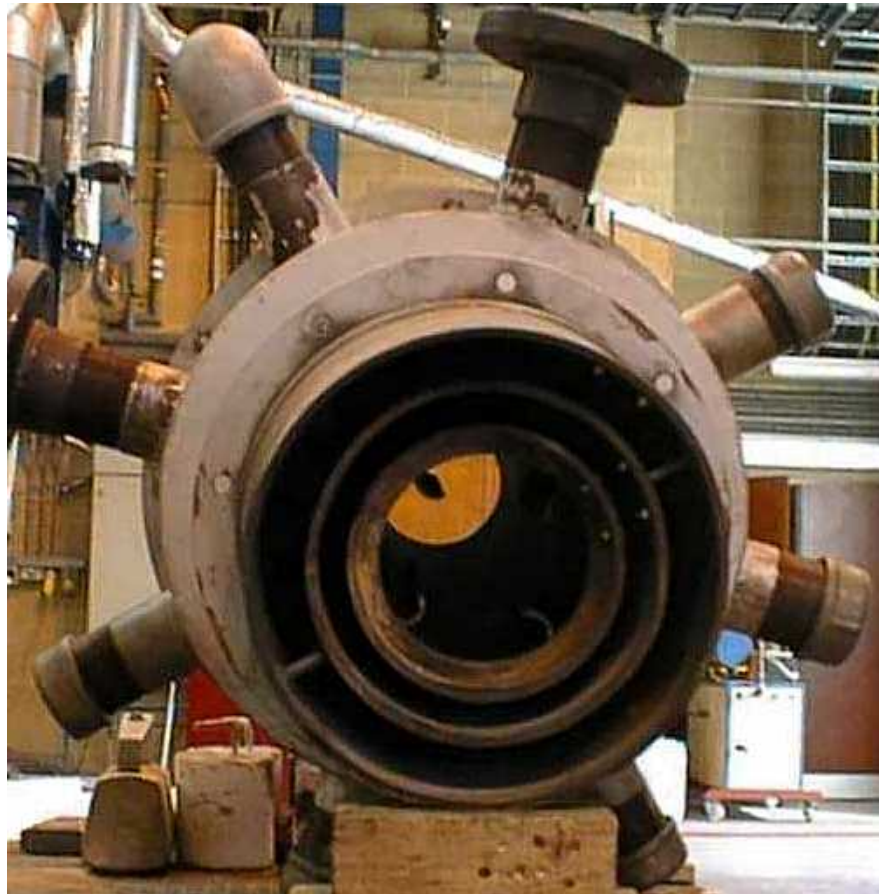


Furnace Geometry

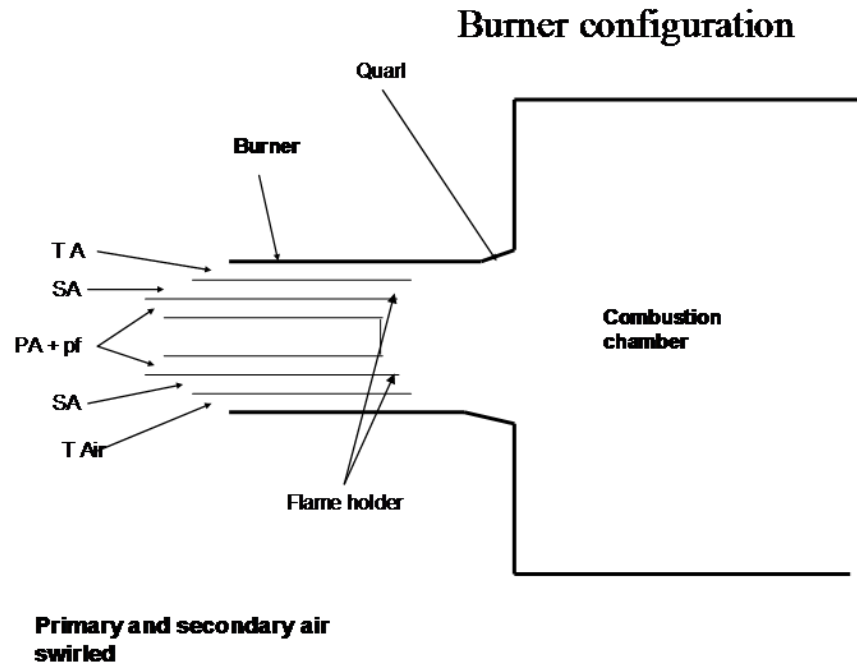
Mitsui Babcock Burner.



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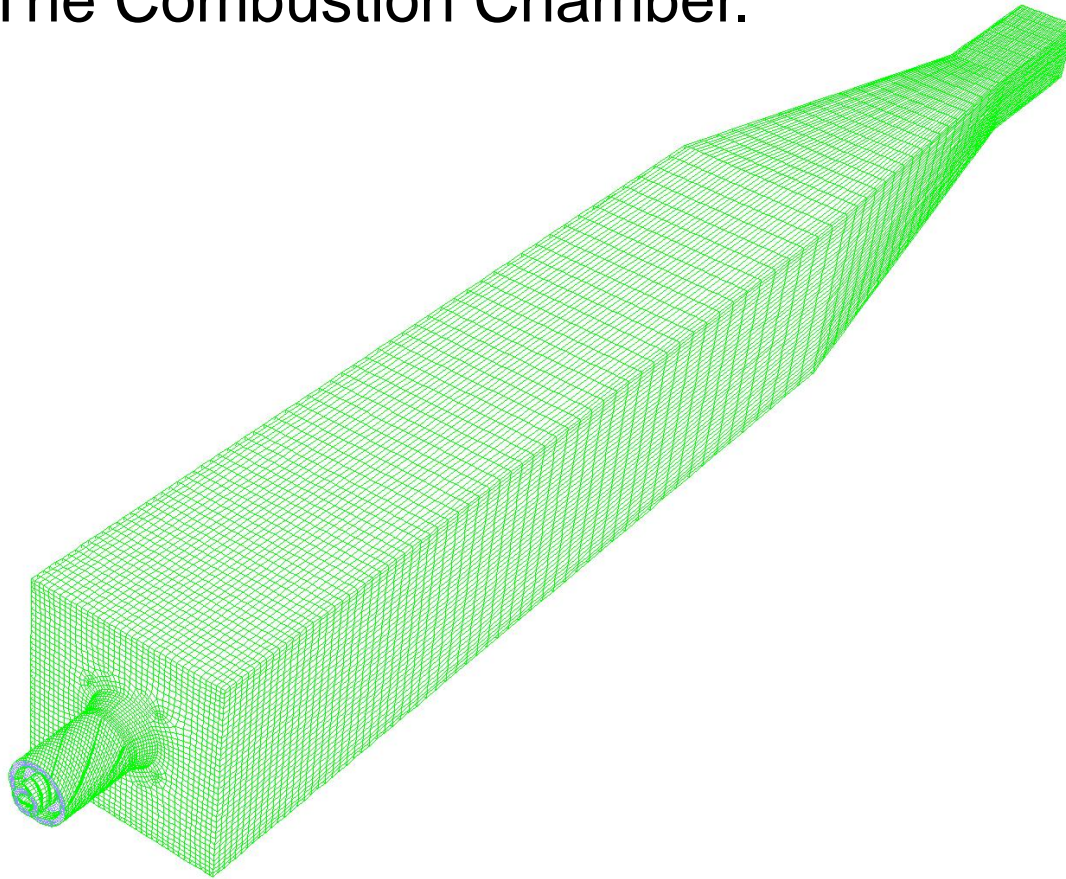


Burner Face Details.



Diagrammatic representation of the Mitsui Babcock Mark III Burner.

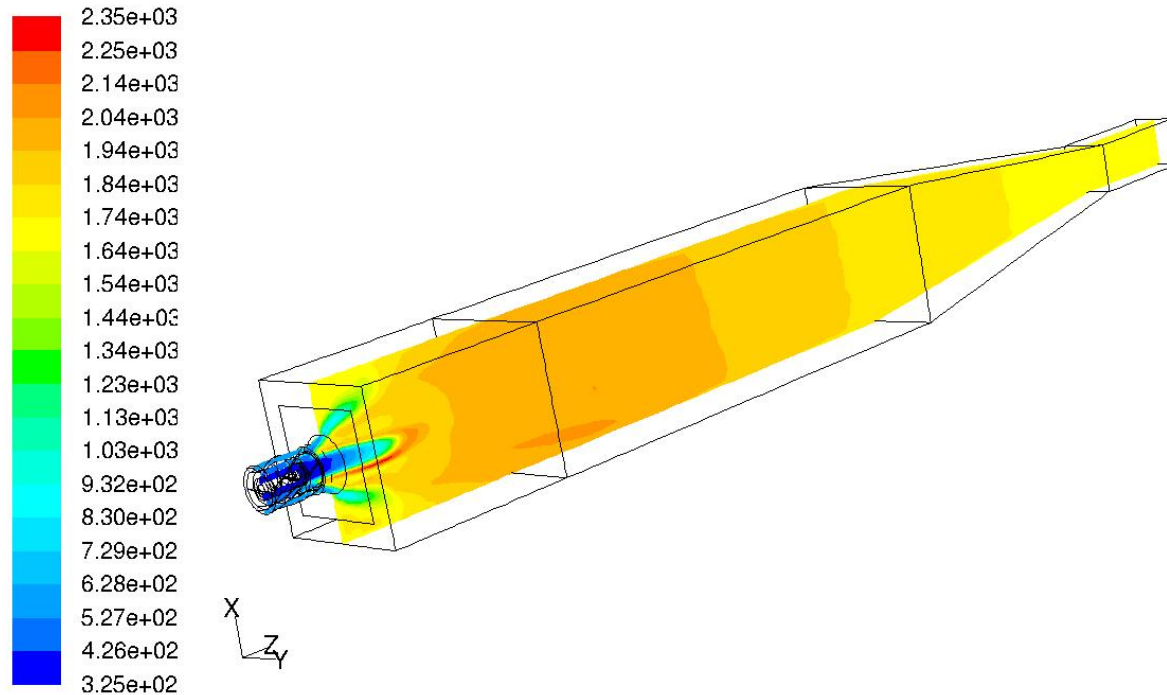
The Combustion Chamber.



Typical Computed Temperatures.



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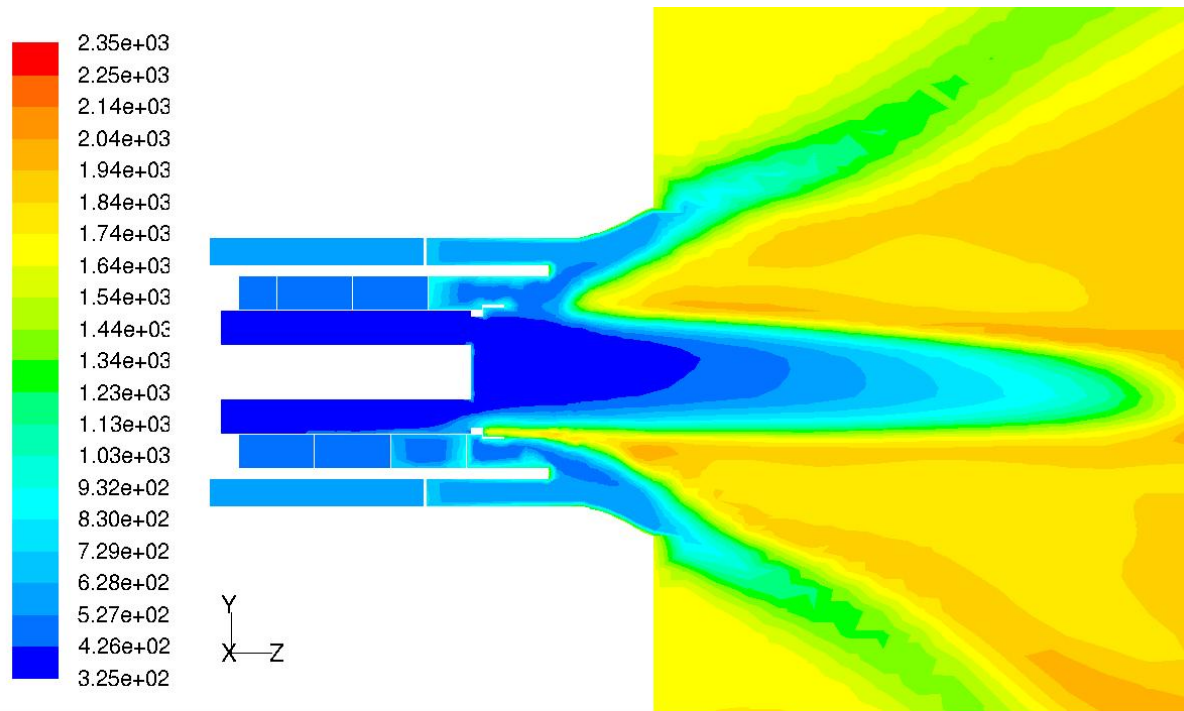
Contours of Static Temperature (k)

Dec 21, 2007
FLUENT 6.3 (3d, dp, pbns, spe, RSM)

Computation of the Near Burner Region.



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Contours of Static Temperature (k)

Jan 11, 2008
FLUENT 6.3 (3d, dp, pbns, spe, RSM)

Photograph of the Flame.



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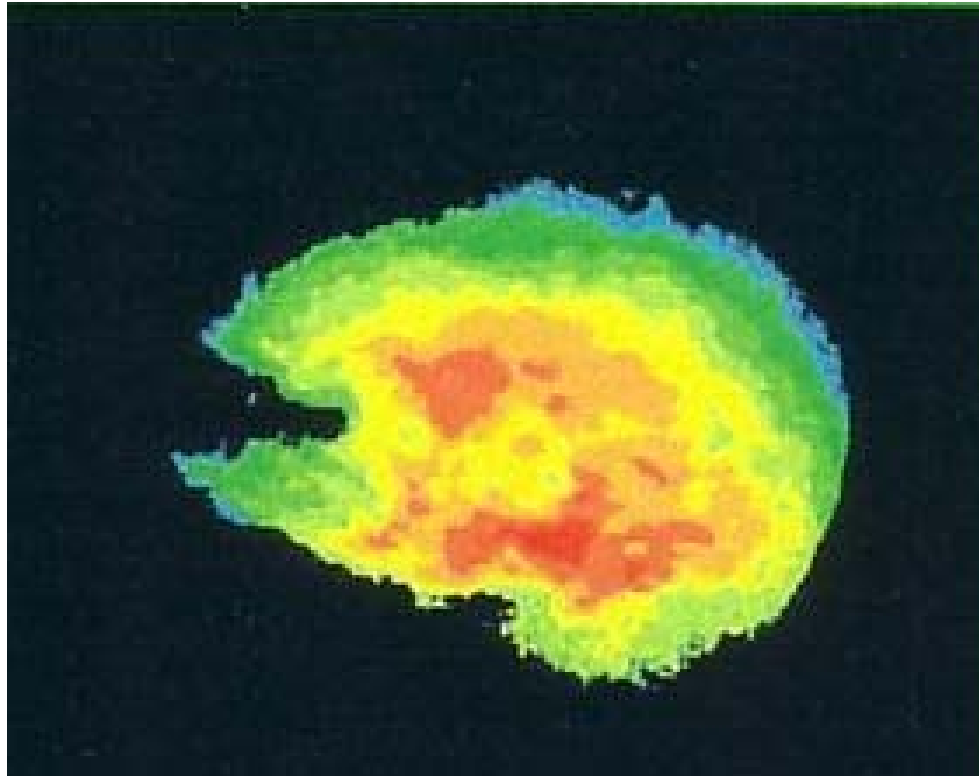


Photograph of the Flame

Measured Temperature Field.



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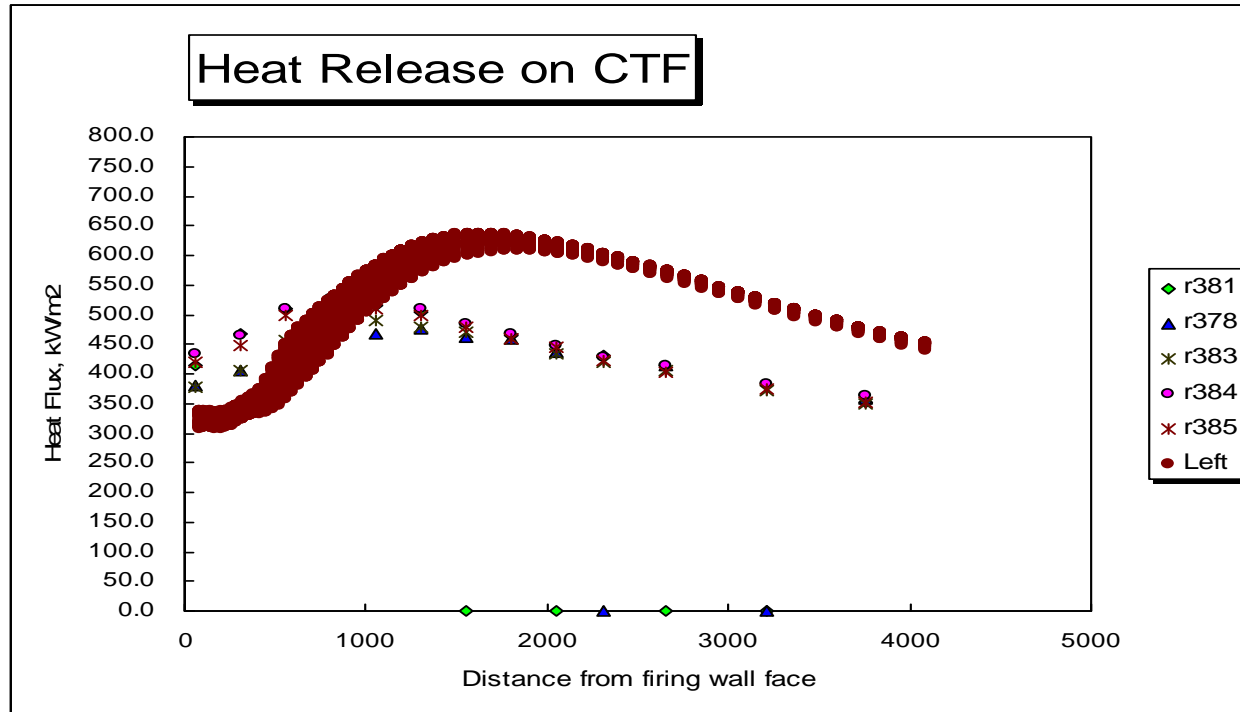


**Measured Temperature Field (Professor Yan):
red 1650°C; yellow, 1580°C; blue/green, 1450°C.**

Measured and Computed Incident Radiation.



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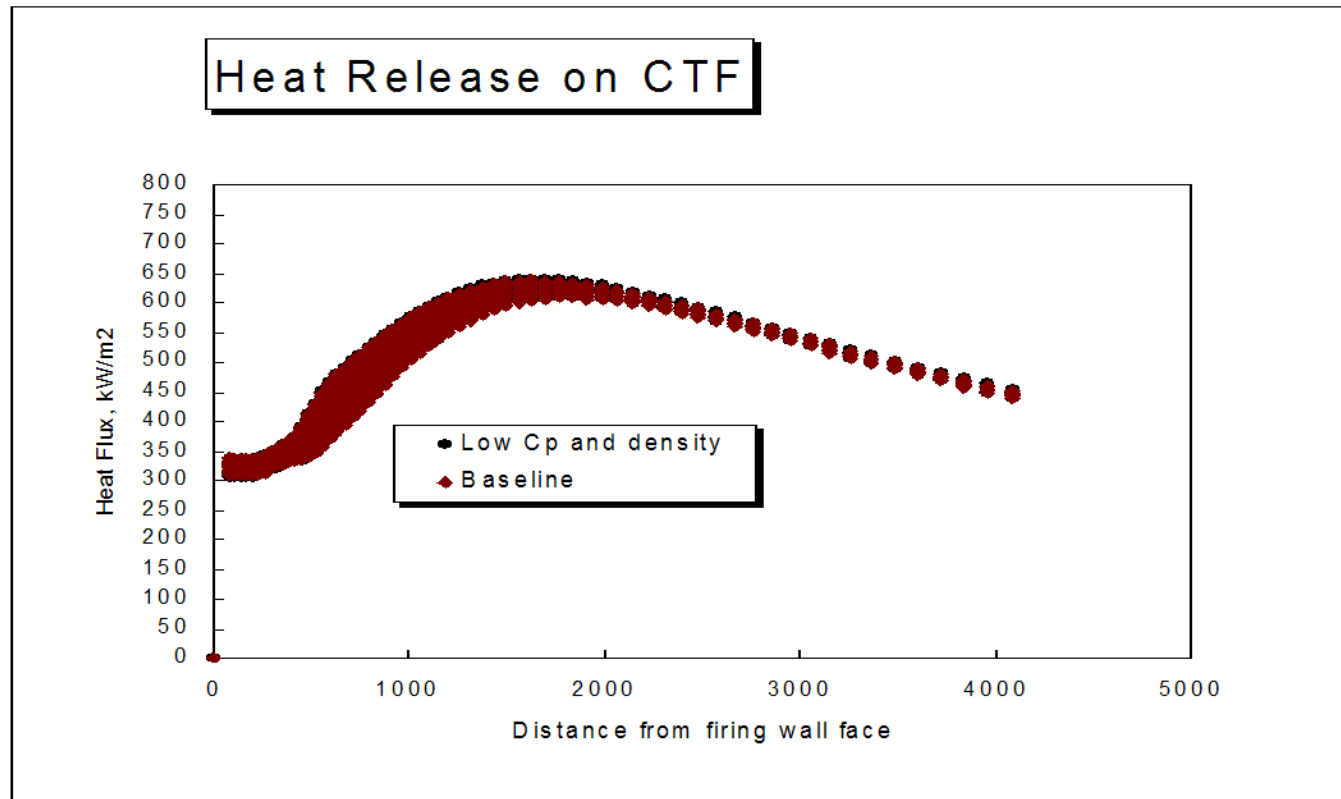


Surface Incident Radiation Measurements and Computed Values for Gascoigne Wood Coal.

Measured and Computed Incident Radiation-Effect of Cp and Density.



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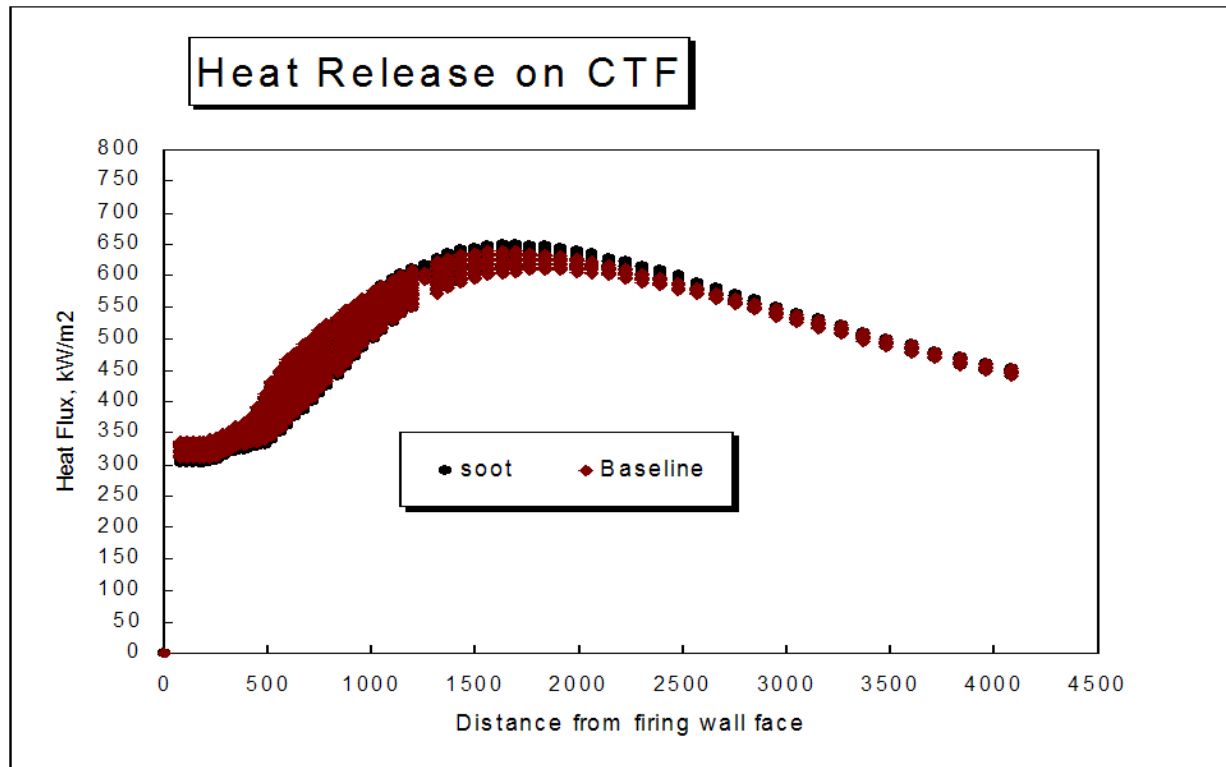


Surface Incident Radiation. Effect of Lowering Cp and Density of Fuel Particles (Gascoigne Wood) (both lowered about 10%).

Effect of Changing Rate of Soot Formation.



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Surface Incident Radiation. Effect of Soot Formation is small (Gascoigne Wood).

Aerodynamic Factors

The drag coefficients, C_D , were calculated as below and shape factors, f , were used to account for the irregular biomass particles shapes.

$$C_D = (24/Re) (1 + b_1 Re^{b_2}) + [b_3 Re / (b_4 + Re)]$$

$$b_1 = 2.3288 - 6.4581f + 2.4486f^2$$

$$b_2 = 0.0964 + 0.5565f$$

$$b_3 = 4.9050 - 13.8944f + 18.4222f^2 - 10.2599f^3$$

$$b_4 = 1.4681 + 12.258f - 20.7322f^2 + 15.8855f^3$$

Examination of Combustion of Single Particles of Biomass.



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Examination of the Combustion of a Single Particle of Wood

There is little disruptive burning. A major issue is the use of equivalent spheres in the combustion model

The NO model used in Fluent permits the N-component in the fuel to be converted to HCN or NH_3 which is then oxidised to NO and N_2 depending on the reaction conditions.

In coal it is known that the fuel-N converts to HCN.

In biomass the fuel-N is in the form of proteins or amino acids and is converted to a mixture of NH_3 + HCN.

For the biomass used here we have allowed it to be converted to 90% NH_3 / 10% HCN which then reacts to form NO.

Co-firing Biomass and Coal.



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Experimental Furnace Flame Shape.

The flame divergence is greater with biomass

Experimental and Computed Results for Single Coals and Co-firing Blends ..



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Fuel	Calc NO ppm (dry)	Measured NO ppm (dry)	Calc C in Ash, Mass %	Measured C in Ash, Mass %	Calculated exit T, K	Experimental Exit T, K
Gascoigne Wood coal	300	325	1.32	3.0	1605	1597
Russian coal	296	325	1.24	3.4	1617	1407
Russian/PKE	316	321	3.5	4.8	1487	1488
S. African coal	292	312	5.87	6.7	1668	1424
S. African coal/ wood	288	319	5.6	5.9	1583	1527
S. African/ Miscanthus (20%)	250	242	8.9	1.94	1664	1470
S. African/ Olive waste (15%)	276	230	0.62	0.98	1646	1539
S. African/Torrefied Wood* (20% thermal)	264	Not available	0.3	Not available	1724	Not available

Comparison of Experimental and Computed Data.

Conclusions

- A coal combustion model has been tested using Gascoigne Wood coal with the RWE npower Combustion Test Facility. Reasonable agreement has been obtained for exit temperatures, NO, unburned carbon-in-ash. However agreement with the radiation measurements is not good. The influence of heating-up of the particles, and the devolatilisation and soot models have been examined, but the key factor seems to be the correct aerodynamic modelling of the burner.
- In the case of biomass the behaviour of water content has been examined and the effect on the release of volatiles from large biomass particles examined.
- Co-firing of wood, miscanthus, PKE and olive wastes with a number of coals has been modelled with reasonable success..